# The Crystal Structure of a Basic Hafnium Chromate

# MARGARETA HANSSON and WANDA MARK

Department of Inorganic Chemistry, Chalmers University of Technology and The University of Göteborg, P.O. Box, S-402 20 Göteborg 5, Sweden

Hafnium chromate of approximate formula  $Hf_4(OH)_8(CrO_4)_4$ .  $H_2O$  crystallizes in space group *Pnnm* with a=11.543, b=13.587, c=6.847 Å and Z=2. It is isotypic with a corresponding zirconium compound with the formula  $Zr_4(OH)_8(CrO_4)_5$ .  $H_2O$ .

with the formula  $\text{Zr}_4(\text{OH})_6(\text{CrO}_4)_5\cdot \text{H}_2\text{O}$ . The crystal structure of the hafnium compound has been determined from X-ray single crystal data by means of three dimensional Fourier syntheses. Least squares refinement of the structural parameters based on 818 independent reflexions yielded a final R value of 0.061.

The hafnium atoms are joined by double oxygen bridges to form planar infinite chains with the composition  $[Hf(OH)_2]_n^{2n+}$ . The chains are connected by chromate groups to form a three-dimensional structure. Seven oxygen atoms are coordinated to each hafnium atom in a pentagonal bipyramidal arrangement. The Hf-O distances range from 2.01 to 2.25 Å.

Some investigations have been performed in order to elucidate the differences between zirconium and hafnium with respect to their chemical behaviour and atomic sizes. The hydrolysis systems  $\rm ZrO_2-SO_3-H_2O$  and  $\rm HfO_2-SO_3-H_2O$  have been investigated by McWhan, Lundgren and Hansson <sup>1,2</sup> and the two systems show discrepancies as regards the conditions under which the different phases are formed.

In the hydrolysis system  $ZrO_2-CrO_3-H_2O$ , three principally different crystalline phases are obtained.<sup>3</sup> In attempts to prepare the corresponding phases in the  $HfO_2-CrO_3-H_2O$  system, only one crystalline phase was found, namely  $4HfO_2.4.3CrO_3.5.4H_2O$ , the corresponding phase in the zirconium system having the composition  $4ZrO_2.4.9CrO_3.3.7H_2O.^3$  Apart from the different compositions of the products, crystallization is more readily brought about in the zirconium system. The crystalline hafnium chromate is formed in very low yield and the crystals are small.

# EXPERIMENTAL

The hafnium chromate investigated was prepared by hydrothermal hydrolysis of an amorphous hafnium chromate in a 10 M chromium trioxide solution at 165°C.

Due to the small amount obtained, the hafnium and chromium contents were determined by electron probe microanalysis. The results indicate an approximate formula of  $\mathrm{Hf_4(OH)_8(CrO_4)_4.H_2O}$ , which can also be written  $4\mathrm{HfO_2.4CrO_3.5H_2O}$ . By refining the structure with three-dimensional X-ray data, it was possible to establish the composition  $4\mathrm{HfO_2.4.3CrO_3.5.4H_2O}$ . The experimental and calculated hafnium and chromium contents are:

	$\%~\mathrm{Hf}$	% Cr
Experimental	53.9	16.2
Calculated for:		
$4 \mathrm{HfO}_{2}.4 \mathrm{CrO}_{3}.5 \mathrm{H}_{2} \mathrm{O}$	53.6	15.6
$4 \mathrm{HfO}_{2}.4 \mathrm{CrO}_{3}.6 \mathrm{H}_{2}\mathrm{O}$	52.9	15.4
4HfO <sub>2</sub> .4.3CrO <sub>3</sub> .5.4H <sub>2</sub> O	52.2	16.3

## PROCESSING OF DATA

From Guinier and Weissenberg photographs it was evident that the hafnium chromate structure is very nearly isomorphous with that of the corresponding zirconium chromate.

The crystals are red truncated double pyramids, that used for the structure determination having a basal plane of  $0.03 \times 0.05$  mm<sup>2</sup> (y and z directions) and a height of 0.05 mm.

Due to the positions of the hafnium atoms in the structure, reflexions with k=2n are very strong while those with k=2n+1 are very weak. The crystal was therefore mounted along the y axis in a single crystal diffractometer (Philips PAILRED) and reflexions from the reciprocal layers h0l-h14l and  $\overline{h}0l-\overline{h}14l$  with k even were registered with MoKa radiation. The  $\omega$  scanning speed was 1°/min, and the total time for registration of one reflexion was 3 min for the lower levels and 6 min for the higher levels. A total of 1196 reflexions were collected with k even. The intensities of the reflexions with k odd are on an average one tenth of those with k even. In order to be able to estimate these weak reflexions with a better accuracy, they were registered with multiple film Weissenberg techniques and  $\mathrm{Cu}K\alpha$  radiation. Each layer  $(h1l-h9l,\ k=2n+1)$  was exposed for 2-3 weeks and the intensities of the 311 independent reflexions thus obtained were estimated visually by comparison with an intensity scale.

# UNIT CELL DIMENSIONS

The crystals have orthorhombic symmetry and the conditions for reflexion are:

h0l with h+l=2n0kl with k+l=2n

The conditions are in accordance with space groups No. 34, Pnn2, and No. 58, Pnnm.

Accurate cell dimensions were obtained by least squares refinement of the cell parameters using the program POWDER.<sup>4</sup> For this purpose 41 lines were indexed on a Guinier powder photograph taken with  $\text{Cu}K\alpha_1$  radiation, using lead nitrate as an internal standard  $(a_{\text{Pb(NO4)}} = 7.8566$  Å at 21°C).<sup>5</sup> The cell dimensions and their standard deviations were found to be (for com-

Table 1. Guinier powder data.  $\lambda_{\mathrm{Cu}K\alpha_1} {=}~1.54050$  Å.

$h \ k \ l$	$10^5 \sin^2  heta \  m obs$	$10^5 \sin^2  heta$ calc	$d \ { m \AA} \  m calc$	$I_{ m obs}$
101	1715	1711	5.8892	${f st}$
120	1734	1731	5.8549	${f st}$
$2\ 0\ 0$	1785	1781	5.7715	$\operatorname{\mathbf{st}}$
$1\ 3\ 0$	3346	3338	4.2162	vvw
(3 1 0	49.41	(4329	3.7021	
$\{2\ 2\ 1$	4341	4332	3.7008	w
`2 3 0	4683	`4673	3.5630	vw
$0\ 0\ 2$	5069	5062	3.4237	$\mathbf{vst}$
0 4 0	5146	5142	3.3968	$\mathbf{vst}$
3 0 1	5274	5273	3.3544	vst
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5299	5293	3.3480	vst
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6801	$\begin{array}{c} 6792 \\ \end{array}$	2.9555	vvw
$\begin{pmatrix} 1 & 2 & 2 \\ 2 & 0 & 2 \end{pmatrix}$		(6843	(2.9446)	V V VV
141	6851		2.9425	$\mathbf{m}$
$\begin{array}{c} 1 & 4 & 1 \\ 2 & 4 & 0 \end{array}$	6934	6852	$\frac{2.9425}{2.9275}$	~ <b>4</b>
		6923		$\mathbf{st}$
4 2 1	9682	9675	2.4763	${f st}$
0 4 2	10195	10203	2.4114	vw
3 2 2	10359	10354	2.3937	vw
3 4 1	10412	10415	2.3868	vw
103	11840	11834	2.2391	w
2~4~2	11990	11984	2.2250	vw
160	12035	12014	2.2222	$\mathbf{w}$
$4 \ 4 \ 0$	12276	12266	2.1993	vw
$5\ 2\ 0$	12433	12417	2.1859	$\mathbf{m}$
$2\ 6\ 1$	14619	14615	2.0148	w
3 0 3	15420	15396	1.9631	w
360	15587	15576	1.9516	$\mathbf{m}$
$\overset{\circ}{1}\overset{\circ}{4}\overset{\circ}{3}$	16969	16975	1.8695	w
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	17077	17076	1.8640	vvw
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	17484	17479	1.8424	w
$\begin{array}{c} 6 & 2 & 2 \\ 6 & 2 & 1 \end{array}$	18581	18580	1.7869	m
$\begin{array}{c} 0 & 2 & 1 \\ 4 & 2 & 3 \end{array}$	19784		1.7311	
		19798		w
461	19944	19959	1.7241	w
0 0 4	20250	20246	1.7118	vw
[0 8 0	20593	$\{20567$	$\{1.6984$	w
$\begin{pmatrix} 3 & 6 & 2 \end{pmatrix}$		(20638	1.6955	••
$\int 1 2 4$	22013	$\int 21977$	$\int 1.6431$	vw
$(2\ 0\ 4)$		122027	(1.6412)	* **
181	22273	22278	1.6319	vvw
$2 \ 8 \ 0$	22351	22348	1.6293	w
560	22727	22701	1.6166	w
$(7\ 0\ 1)$	99000	(23083	(1.6032)	<b></b>
<b>720</b>	23090	23103	$\{1.6025$	$\mathbf{m}$
263	24740	24738	1.5486	vvw
$(3\ 2\ 4)$		(25539	(1.5242	
$\{ \begin{array}{cccccccccccccccccccccccccccccccccccc$	25571	$\{25629$	1.5215	vw
$\overset{(0}{2}\overset{0}{4}\overset{2}{4}$	27176	27169	1.4777	vvw
$\begin{array}{c} 2 & 4 & 4 \\ 5 & 6 & 2 \end{array}$	27741	$\begin{array}{c} 27763 \\ 27762 \end{array}$	1.4619	vvw
$\begin{array}{c} 3 & 0 & 2 \\ 6 & 2 & 3 \end{array}$	28716	28703	1.4377	vw
U 4 0	40110	40100	1.40//	v w

parison those of the corresponding zirconium compound are given within brackets):

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a = 11.543 \pm 0.002 \text{ Å} (11.629)

b = 13.587 \pm 0.002 \text{ Å} (13.653)

c = 6.847 \pm 0.001 \text{ Å} (6.882)

V = 1073.9 + 0.3 \text{ Å}^3 (1092.7)
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The observed and calculated values of  $\sin^2\theta$  less than 0.30 are listed in Table 1, together with the calculated inter-planar spacings. As the experimental density could not be determined, the number of formula units per unit cell was assumed to be Z=2 as in the corresponding zirconium chromate structure. On the basis of this assumption, the calculated density is 4.18 g/cm³, which seems reasonable.

#### STRUCTURE DETERMINATION AND REFINEMENT

The two sets of data were corrected for Lorentz, polarization and absorption effects with the programs DATAP1 and DATAP2,6 respectively. To bring the different data sets on to the same scale, a structure factor calculation was performed, which was based on the hafnium atoms, assuming that the positional parameters were the same as in 4ZrO<sub>2</sub>.4.9CrO<sub>3</sub>.3.7H<sub>2</sub>O. Successive three dimensional Fourier syntheses were calculated (program DRF 6) to obtain the positions of the chromium and oxygen atoms. In the calculations, the space group Pnnm was used and the positions of the atoms labelled  $Cr_1$ ,  $Cr_2$ ,  $O_1 - O_{10}$ , and O<sub>12</sub> could be determined without any ambiguity. All atoms occupy the special position 4(g) except  $O_1$  and  $O_2$  which are situated in the general position 8(h). This implies the composition  $Hf_4(OH)_8(CrO_4)_4.2H_2O$  or  $4HfO_2.4CrO_3$ . 6H<sub>2</sub>O. The O<sub>12</sub> atoms correspond to the two water molecules of crystallization per formula unit. A Fourier synthesis, based on the refined atomic parameters, showed small excesses of electron density at very nearly the same positions as the Cr<sub>3</sub> atoms in the zirconium chromate structure. It was therefore considered likely that the hafnium compound contained a small additional amount of chromate (Cr<sub>3</sub>). These chromate groups must be statistically distributed between four equivalent positions, as will be seen later. As the additional chromate oxygen atoms (O<sub>11</sub>) could not be located from the Fourier syntheses, they were assumed to occupy the same positions as in the zirconium structure. Refinement of the parameters was performed with the program BLOCK, 6 different occupation numbers being assigned to Cr<sub>3</sub>. In the different refinements, the occupation number of O<sub>11</sub> was assigned the same value, q, as that of  $Cr_3$ . The occupation number for  $O_{12}$ , (1-q), (cf. later) was deduced from the positional relationship between Cr<sub>3</sub> and O<sub>12</sub>. The best fit with the experimental data was obtained for an occupation number of 0.14 for  $Cr_3$  and thus of 0.86 for  $O_{12}$ .

A few cycles of refinement with the least squares full matrix program LINUS 6 showed that secondary extinction effects were of little importance. The final cycles of refinement were performed with the program LALS.6

Table 2. Observed and calculated structure factors for  $\sim \mathrm{Hf_4(OH)_8(CrO_4)_4.H_2O.}$ 

H 0 0 2 513 457 6 150 -131 8 211 -187 10 350 -335	H 0 11 1 105 111 3 105 100 9 95 -87	9 125 -125 13 84 89 H 2 9 4 160 -165	H 4 8 0 237 -228 2 141 -149 10 154 157 12 129 136	H 6 B 3 155 152 5 175 173 7 119 129 9 94 88	H 8 9 1 154 162 9 96 -101 H 8 10
10 330 -335 12 289 -266 14 104 -93 20 87 82 22 78 90 H 0 1	H 0 12 0 126 144 10 95 -84 12 80 -75 H 0 13	6 192 -196 8 99 -59 H 2 10 3 146 -136 5 118 -137	F 4 9 1 148 -153 3 125 -129 7 97 87 9 127 125	H 6 9 2 94 92 4 153 160 6 156 158 8 101 88	0 132 152 2 122 115 10 126 -101 H 8 11 1 105 112
1 448 432 3 478 455 5 70 65 7 359 -314 9 27C -258 11 187 -184	1 94 84 H 0 14 D 96 99	7 111 -110 H 2 11 4 109 -113 6 131 -137	11 113 113 13 86 80 H 4 10 O 189 -187 2 119 -122	H 6 10 3 118 126 5 133 143 7 110 103 9 94 63	H 10 0 3 214 -216 5 405 -394 7 285 -283 9 105 -108
13 181 -169 15 134 -116 F 0 2 0 803 816	1 291 -296 3 501 -493 5 490 -453 7 314 -314 9 271 -255	H 2 12 3 85 -83 H 4 0 2 377 -383 4 215 -208	10 118 126 H 4 11 1 110 -104 3 98 -90	H 6 11 4 104 109 6 118 111	13 93 97 15 151 141 17 121 122 H 10 1 1 33 -25
8 110 -113 10 294 -282 12 256 -245 14 103 -100	13 204 188 15 184 177 17 106 110 H 2 1 2 108 -112 4 372 -380	6 86 74 8 228 223 10 343 331 12 273 260 14 94 54	H 4 12 0 133 -119 2 95 -76 H 6 0 1 206 249	2 334 333 4 179 180 6 98 -69 8 250 -231 10 261 -252 12 204 -191	2 204 -213 4 253 -245 6 254 -252 8 236 -219 10 107 -91 12 113 92
H 0 3 1 453 454 3 399 405 5 65 51 7 317 -310 9 267 -265 11 177 -186	6 524 -509 8 236 -223 14 123 120 16 194 183 18 120 118	H 4 1 1 315 -345 3 329 -337 5 161 -144 7 192 167 9 295 262	3 476 454 5 442 426 7 270 269 9 169 164 13 133 -129 15 159 -153	12 204 - 191 14 114 - 105 20 99 80 H 8 1 1 350 378 3 222 220	14 154 137 16 111 116 H 10 2 1 68 -26 3 155 -153
11 177 -186 13 148 -153 15 125 -100 19 88 93 21 82 80	H 2 2 1 205 -212 3 298 -311 5 319 -316 7 249 -255 9 268 -248	11 253 243 13 156 159 15 84 £1 19 93 -84	17 148 -125 H 6 1 2 232 233 4 396 393 6 377 374	7 144 - 130 9 219 - 209 11 235 - 232 13 158 - 151	5 325 - 327 7 240 - 248 9 105 - 107 13 97 79 15 141 128 17 128 119
0 631 661 2 256 304 6 85 -72 8 135 -132 10 251 -263 12 212 -221	13 166 158 15 157 159 17 105 108 19 88 77	0 457 -461 2 250 -264 4 161 -171 8 158 153 10 287 282 12 257 240	8 165 170 16 178 -157 18 109 -106 H 6 Z 1 192 189	0 374 369 2 248 258 4 148 159 8 193 -179 12 185 -176 14 127 -109	H 10 3 2 208 -213 4 241 -259 6 244 -249 8 211 -205
14 95 -85 H C 5 1 250 266 3 255 269 5 80 61	2 173 -161 4 412 -415 6 478 -480 8 209 -211 12 89 78 14 122 122	14 117 101 H 4 3 1 382 -384 3 309 -320 5 111 -108	3 313 321 5 320 326 7 215 225 9 177 163 15 146 -138 17 141 -122	H 8 3 1 383 383 3 206 214 7 137 -144 9 205 -212	10 87 -75 12 110 95 14 147 135 16 115 111 H 10 4
7 195 -193 9 182 -189 11 136 -144 13 134 -135 15 100 -96 19 80 79	16 176 172 18 104 107 H 2 4 1 188 -189 3 321 -317	7 201 207 9 277 260 11 236 234 13 133 145	H 6 3 2 242 241 4 384 399 6 344 362 8 166 167	11 220 -224 13 151 -139 17 89 33 H 8 4 0 346 347	3 149 -163 5 301 -303 7 225 -227 9 85 -93 15 116 119 17 104 108
+ 0 6 0 430 466 2 230 239 8 96 -113 10 200 -216	5 304 -310 7 233 -240 9 207 -205 13 163 150 15 146 148 17 99 96	0 440 -443 2 275 -272 4 139 -139 8 155 160 10 261 262 12 214 215	14 132 -120 16 173 -149 H 6 4 1 164 161 3 303 302	2 247 250 4 149 139 8 179 -175 10 202 -204 12 168 -160	H 10 5 2 145 -148 4 178 -181 6 178 -187 8 166 -165
12 182 -183 H 0 7 1 233 245 3 198 213 7 169 -169	H 2 5 2 80 -80 4 254 -260 6 337 -338 8 163 -165	14 87 86 H 4 5 1 227 -237 3 213 -223 5 91 -93	5 304 312 7 218 214 9 136 138 13 94 -104 15 126 -129 17 114 -110	H 8 5 1 249 261 3 154 155 7 97 ~89 9 157 ~156 11 189 ~179	14 114 108 H 10 6 3 130 -139 5 235 -246 7 191 -187
9 171 -173 11 124 -128 13 105 -106 15 87 -70 H C 8	14 99 91 16 149 147 H 2 6 1 146 -140 3 249 -250	7 128 129 9 199 201 11 175 182 13 124 129 15 88 69	H 6 5 2 142 148 4 249 261 6 258 261 8 132 136 14 102 -92	13 120 -122 H 8 6 0 258 275 2 199 202 4 106 111 8 154 -145	15 109 101 H 10 7 2 116 -132 4 158 -170 6 162 -165 8 131 -134
0 263 295 2 142 160 8 79 -70 10 149 -156 12 133 -140 H 0 9	5 226 - 246 7 190 - 195 9 146 - 162 13 109 125 15 124 125	9 343 -346 2 220 -219 4 94 -104 8 133 132 10 215 216 12 181 177	14 102 -92 16 133 -127 18 96 -88 H 6 6 1 112 118 3 240 235	10 166 -170 12 153 -134 H 8 7 1 227 232 3 105 133	H 10 8 5 164 -174 7 131 -137
H C 9 1 151 165 3 140 146 7 114 -114 9 136 -122 H C 10	H 2 7 2 88 -96 4 244 -242 6 277 -280 8 137 -135 16 129 123	12 181 177 14 82 71 H 4 7 1 221 -224 3 182 -185 7 148 126	5 240 251 5 241 251 7 169 177 9 109 111 15 94 -110	9 148 -142 11 157 -153 H 8 8 0 177 184 2 134 141	4 122 -121 6 101 -118 8 101 -100 H 10 10 3 85 -84
0 226 229 2 130 131 10 121 -126 12 108 -107	H 2 8 1 87 -94 3 151 -161 5 145 -164 7 139 -139	9 182 178 11 134 154 13 91 102	2 134 137 4 229 233 6 228 224 8 125 116 16 101 -106	4 81 82 8 90 -99 10 112 -124 12 98 -103	5 140 -141 H 10 11 2 79 -65 6 98 -84

Table 2. Continued.

H 12 C 2 256 -265	H 14 4 3 141 145 5 228 239 7 169 171	716*	7 33 28	13 16 -17	6 62 -51
4 180 -169	5 228 239	9 39 -36	9 76 75	H 5 3	8 - 4+
4 180 -169 6 89 83 8 218 215	7 169 171	8 26 30 9 39 -36 10 50 59 114*	10 - 6*	0 23 28	9 34 -30
2 256 -265 4 180 -169 6 89 83 8 218 215 10 182 181	H 14 5	716* 8 26 30 9 39 -36 10 50 59 114* 12 33 45 13 21 42	7 33 28 8 - 8* 9 76 75 10 - 6* 11 56 62 1214* 13 12 15	2 - 18*	6 62 -51 7 80 -65 8 - 4* 9 34 -30 10 - C* 11 43 44 12 62 -66
H 12 C 2 256 -265 4 180 -169 6 89 83 8 218 215 10 182 181 12 110 132	2 153 146 4 157 160	13 21 42	7 33 28 8 - 8* 9 76 75 10 - 6* 11 56 62 1214* 13 12 15	3 57 57	12 62 -66
	6 121 128	H 1 5	н з 4	0 23 28 1 24 26 2 - 18* 3 57 57 4 20 -28 5 43 -36 6 68 57 7 74 -63	H 7 3
1 316 -332	8 125 119	09*	1 34 41	6 68 57	0 54 54
F 12 1 1 316 -332 3 133 -131 7 75 74 9 168 160 11 218 208 13 122 126	H 14 6 3 125 122 5 204 200	26*	315*	8 72 66	2 34 -25
9 168 160 11 218 208	3 125 122 5 204 200	3 25 -25	42*	9 25 -25	325*
1 316 -332 3 133 -131 7 75 74 9 168 160 11 218 208 13 122 126	7 146 144	H 1 5 099 1129 264 3 25 -25 4 - 55 5 - 158 6 38 -44 7 29 33 8 27 -34 9 - 10° 10 - 0° 11 19 30	H 3 4 1 34 41 2 53 -62 315* 42* 5 21 15 6 30 35 7 59 60 8 - 6* 9 34 40 10 34 34 11 29 -34 12 54 69	H 5 3 0 23 28 1 24 26 2 - 18* 3 57 57 4 20 -28 5 43 -36 6 68 57 7 74 -63 8 72 66 9 25 -25 103* 11 42 -50 12 33 -42 13 35 -57	F 7 3 0 54 54 1 40 -41 2 34 -25 3 -25* 4 105 -106 5 84 72 6 -13* 7 -8* 8 - 12* 9 67 -66 10 25 -14 11 52 -59
	H 14 7	6 38 -44	7 59 60 8 - 6*	12 33 -42 13 35 -57	613*
0 257 -241	H 14 7 2 133 128 4 130 145 6 107 115 8 106 100	8 27 -34	9 34 40	., ,, ,,	8 - 12*
2 218 -222 4 141 -155 8 183 180 10 147 157	4 130 145 6 107 115	9 - 10*	10 34 34 11 29 -34	H 5 4	9 67 -66
8 183 180	8 106 100	11 19 30	12 54 69	2 39 -43	10 25 -14 11 52 -59
H 12 2 0 257 -241 2 218 -222 4 141 -155 8 183 180 10 147 157 12 111 122	H 14 8 5 152 148 7 98 109	H 1 6	н 3 5	3 47 50 4 - 13#	H 7 A
	5 152 148	1 - 8*	0 33 -38	5 52 53	1 54 -58
H 12 3 1 330 -326		2 - 10*	1 26 31 2 18 16	6 20 20 71*	2 78 79 3 19 23
3 132 -131	h 14 9 2 90 93 4 105 105 6 88 84	47*	3 - 6*	8 39 -38	4 - 5*
9 177 161	2 90 93 4 105 105 6 88 84	529* 6 - 1*	4 43 52 5 39 -52	9 - 13* 10 75 -85	58* 6 45 -47
1 330 -326 3 132 -131 7 83 85 9 177 161 11 207 201 13 115 117	h 14 9 2 90 93 4 105 105 6 88 84	716*	6 24 20	11 25 29	7 60 -62
13 117 117	н 1 0	H 1 6 1 - 8* 2 - 10* 329* 47* 529* 6 - 1* 716* 8 - 26* 9 20 -28 10 30 45	0 33 -38 1 26 31 2 18 16 3 - 6* 4 43 52 5 39 -52 6 24 20 7 - 9* 8 - 0* 9 42 48	1Z Z5 -36	6 62 -51 7 80 -65 8 - 49 9 34 -30 10 - 62 11 43 44 12 62 -66 7 7 3 0 54 54 1 40 -41 2 34 -25 3 105 -106 5 8 - 128 8 - 128 9 67 -66 10 25 -14 11 52 -59 17 4 54 -58 2 7 6 58 10 54 54 54 7 7 -66 10 25 -14 10 54 54 58 10 54 56 58 10 64 58 68 10 68 68 68 68 68 10 68 68 68 68 68 10 68 68 68 68 68 68 68 68 68 68 68 68 68
F 12 4	2 30 30	10 30 49	9 42 48	H 5 5	105*
0 233 -232 2 207 -209	412*		1 34 41 2 53 -62 3 -15* 42* 5 21 15 6 30 35 7 59 60 8 - 6* 9 34 40 10 34 34 11 29 -34 12 54 69  H 3 5 0 33 -38 1 2 18 16 31 2 18 16 3 - 6* 4 43 52 5 39 -52 6 24 20 7 - 9* 8 - 0* 9 42 48 10 - 11* 11 31 45	0 - 18* 1 - 15*	11 34 46
4 135 -138	5 99 -70	07*		2 - 6*	H 7 5
P 12 4 C 233 -232 2 207 -209 4 135 -138 6 79 61 8 171 172 10 149 150	2 30 30 3 100 -71 412* 5 99 -70 61* 7 27 -16 8 61 53 9 64 -8 111 - 2* 12 56 57 13 62 58 14 16 18	H 1 7 0 - 7-7* 112* 27* 3 18 -19 47* 5 - 9* 6 27 -40 7 22 33 8 17 -27 H 3 C 1 70 68 2 117 -104 3 11 -34 4 - 7* 5 61 39 6 68 52 7 108 84 8 21 17 9 57 73 10 64 47 11 51 -50 12 93 85 13 69 -60 14 29 31	H 3 6 1 19 28 2 32 -42 364 434 5 -144 6 22 26 7 36 46 88* 9 24 32 10 17 28 H 3 7 C 18 -24 116* 212* 34* 4 33 46 5 24 -34 6 21 26 7 14 16	h 5 4 1 40 -37 2 39 -43 3 47 50 4 -13** 5 52 5** 6 20 20 7 -1** 10 75 -85 11 25 29 12 25 -36  h 5 5 2 7 -36  h 5 6 1 -15** 3 34 35 5 25 -36  h 5 6 1 -15** 3 34 35 5 25 -31 2 4 -31 3 29 39 4 -31 3 29 39 4 -10** 5 30 40 6 -15** 7 -10** 8 23 -34 9 -11** 1 24 -28 2 27 -31 3 29 39 4 -10** 5 30 40 6 -15** 7 -10** 8 23 -34 9 -11** 1 18** 2 - 7** 3 - 18** 1 24 -28 2 27 -31 3 29 39 4 - 10** 5 30 40 6 - 15** 7 - 18** 1 24 -28 2 27 -31 3 29 39 4 - 10** 5 30 40 6 - 15** 7 - 18** 1 24 -28 2 - 7** 3 - 28** 4 - 10** 3 - 28** 4 - 10** 5 18 -24 6 24 37 7 23 -37	0 33 36 1 27 -29
10 149 150	8 61 53	3 18 -19	1 19 28 2 32 -42 36* 43* 5 - 14* 6 22 26 7 36 46 8 - 8* 9 24 32 10 17 28	5 25 -32	2 20 -23
H 12 5	10 94 81	5 - 91	43*	7 34 -38	4 63 -69
1 248 -241 3 110 -98 9 126 122 11 169 164 13 111 103	11 - 2*	6 27 -40	5 - 14*	8 46 53	5 54 60
3 110 -98 9 126 122 11 169 164 13 111 103	13 62 58	8 17 -27	7 36 46	10 - 4*	7 - 3*
11 169 164 13 111 103	14 16 18	н з с	8 - 8* 9 24 32	11 21 -31	8 - 16*
	F 1 1	H 3 C 1 70 6E 2 117 -104 3 41 -34 4 - 7* 5 61 39 6 68 52 7 108 68 52 7 108 42 8 21 17 9 57 53 10 64 47 11 51 -55 12 93 85 13 69 -60 14 29 31	10 17 28	H 5 6	, 42 -40
H 12 6 O 179 -192 2 186 -172	0 21 -25 1 19 -23 2 10 -11 3 72 -56 4 17 21 5 38 33 6 99 -74 7 70 55 8 66 -53 9 31 12	2 117 -104 3 41 -34	H 3 7	1 24 -28 2 27 -31	H 7 6
0 179 -192 2 186 -172 4 112 -113 8 135 143 10 119 127 12 104 95	2 10 -11	7*	0 18 -24	3 29 39	2 47 57
4 112 -113 8 135 143 10 119 127 12 104 95	3 72 -56 4 17 21	5 61 39 6 68 52	1 - 16* 2 - 12*	4 - 10* 5 30 40	3 - 14* 4 - 5*
10 119 127	5 38 33	7 108 84	3 - 4*	6 - 15*	510+
	6 99 -74 7 70 55	8 21 17 9 57 53	4 33 46 5 24 -34	7 - 0* 8 23 -34	6 30 -36 7 39 -49
H 12 7	8 66 -53	10 64 47	0 18 -24 1 - 16* 2 - 12* 3 - 4* 4 33 46 5 24 -34 6 21 26 7 14 16	9 - 11+	67*
H 12 7 1 210 -210 3 84 -88 9 128 111 11 159 141	10 - 7*	1 70 68 2 117 -104 3 41 -34 4 - 7* 5 61 39 6 68 52 7 108 84 8 21 17 9 57 53 10 64 47 11 51 -50 12 93 85 13 69 -60 14 29 31	7 14 16	H 5 7	H 7 7
9 128 111 11 159 141	11 40 44	13 69 -60	F 5 0	0 - 19*	0 21 26
11 157 141	1 1 0 21 -25 1 19 -23 2 10 -11 3 72 -56 4 17 21 5 38 33 6 99 -74 7 70 55 8 66 -53 9 31 12 10 - 7 ** 11 4C 44 12 23 20 13 45 47 14 18 21	14 29 31	+ 5 0 1 33 -42 2 36 -46 3 70 67 4 - 17* 5 108 82 6 31 27 73* 8 74 -58 9 1 - 13* 10 132 -114 11 40 28 12 48 -47 13 32 -30	2 - 7*	216*
H 12 8 O 131 -132 2 115 -124 8 89 103	14 18 21	F 3 1	3 70 67	3 - 28*	312*
0 131 -132 2 115 -124	H 1 2	1 62 70	5 108 82	5 18 -24	5 28 40
	2 32 40	2 31 28	6 31 27 73#	6 24 37	нас
H 12 9 1 145 -151 3 71 -63	3 51 -47	4 114 93	8 74 -58		1 51 60
1 145 -151 3 71 -63	5 39 -34	6 44 29	10 132 -114	H 7 0 1 67 -80	2 61 59 3 65 -67
	610*	7 28 18	11 40 28	2 111 115	4 27 -26
F 12 10 0 100 -111 2 57 -101	8 29 20	9 89 71	13 32 -30	44*	612*
2 57 -101	1   1   0   21   -25   1   19   -23   2   10   -11   3   72   -15   4   17   2   3   3   3   3   3   3   3   3   4   7   14   18   2   1   2   2   3   2   4   2   3   5   1   4   4   4   5   3   9   5   1   4   5   6   5   6   5   8   9   9   5   1   4   5   6	H 3 1 C 78 -88 1 62 70 2 31 28 3 - 13* 4 114 93 5 102 -5C 6 44 29 7 28 18 8 - 2* 9 89 71 10 - 12* 11 68 62 121* 13 21 15	F 5 1	5 34 -23 6 80 -47	7 - 5* 8 70 71
H 14 0	1114*	121*	0 - 16*	7 103 -83	9 29 -15
1 31 47 3 188 186	12 44 46 13 43 39	13 21 15 14 36 -43	1 11 12	812*	10 82 88
3 188 186 5 296 294 7 201 206 15 106 -108	14 17 23		3 74 65	10 24 -7	12 - 23+
H 14 0 1 31 47 3 188 186 5 296 294 7 201 206 15 106 -108	H 1 3	1 56 59	H 3 6 1 19 28 2 32 -42 36* 43* 5 - 1-8* 6 22 26 7 366 46 7 366 46 1 - 12* 34* 4 33 46 5 24 -34 6 7 14 16 1 33 -44 1 33 6 -46 3 10 17 5 108 82 6 31 27 73* 8 74 -58 9 - 11* 11 40 28 11 12 2 32 22 3 32 -30 1 11 12 2 32 22 3 74 65 4 39 -46 5 78 3 -59 8 91 74 6 78 3 -59 8 91 74 911* 10 - 3* 8 91 74 6 77 83 -59 8 91 74 911* 10 - 3* 8 91 74 6 78 3 -59 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 8 91 74 911* 10 - 3* 11 50 -44 12 38 -50 13 55 -60	H 7 0 1 67 -80 2 111 115 3 33 33 34 -23 5 34 -23 6 80 -67 7 103 -83 8 - 120 9 36 -35 10 24 -7 11 70 62 12 83 -71 13 34 41	H 9 1
	0 18 -22	2 83 -83	6 77 56	13 34 41	0 33 -40
2 193 196 4 225 214	210*	3 33 -31 42*	7 83 -59 8 91 74	H 7 1	1 29 -33 2 - 0*
H 14 1 2 193 196 4 225 214 6 168 168 8 136 149 10 97 77 14 110 -113 16 108 -90	3 42 -44	5 - 3*	911+	0 54 66	3 55 -51
8 136 149	5 22 25	7 80 64	11 50 -44	2 41 -33	5 89 72
6 168 168 8 136 149 10 97 77 14 110 -113 16 108 -90	6 75 -73 7 63 60	87* 9 53 48	10 - 3* 11 50 -44 12 38 -36 13 55 -60	3 16 -26 4 132 -110	6 75 -60 7 52 42
16 108 -90	8 46 -48	10 45 30		5 111 91	8 96 -83
	9 31 29 10 - 10*	11 29 -30 12 76 76	H 5 2 1 48 -52	6 - 1* 7 - 0*	9 - 2* 10#
+ 14 2 3 142 149 5 258 256 7 184 184 15 102 -98	H 1 3 0 18 -22 1 28 -29 2 10* 3 42 -44 45* 5 22 25 6 75 -7 6 3 60 8 46 -48 9 31 29 10 10* 11 37 48 12 21 30 44	+ 3 2 1 56 59 2 83 -83 3 35 -37 42* 5 - 3* 6 46 36 7 80 64 36 87* 9 53 46 10 45 30 11 29 -30 12 76 76 13 43 -39 14 24 36	1 48 -52 2 50 -61 3 55 50 4 - 11* 5 71 58	H 7 1 0 54 66 1 46 -55 2 41 -33 3 16 -26 4 132 -110 5 111 91 6 - 1* 7 - 0* 8 26 20 9 80 -65 1021* 11 70 -61	11 50 44
3 142 149 5 258 256 7 184 184	12 21 30 13 30 44		3 35 50 4 - 11*	9 80 -65 1021*	12 35 40
15 102 -98		H 3 3	5 71 58	H 7 1 0 54 66 1 46 -55 2 41 -33 3 16 -26 4 132 -110 5 111 91 6 - 1* 7 - 0* 8 26 20 9 80 -65 1021* 11 70 -61	F 9 2
H 14 3	H 1 4 1 - 15* 2 - 20*	1 38 44	0 34 31 75*	H 7 2	2 70 66
2 191 192 4 224 215 6 177 167	1 - 15* 2 - 20* 3 40 -41 410* 5 33 -37	0 51 -61 1 38 44 2 23 20 3 - 11* 4 91 92 5 67 -69	8 33 -29	H 7 2 1 76 -77 2 104 105 3 38 38 4 - 8* 5 - 4*	3 58 -53 4 25 -19
6 177 167	410*	4 91 92	10 98 -88	3 38 38	5 62 -51
2 191 192 4 224 215 6 177 167 8 138 143 14 128 -111	H 1 4 1 - 15* 2 - 20* 3 40 -41 410* 5 33 -37 61*	H 3 3 0 51 -61 1 38 44 2 23 20 3 - 11* 4 91 92 5 67 -69 6 44 41	F 5 2 1 48 -52 2 50 -61 3 55 50 4 - 11* 5 71 58 6 34 31 75* 8 33 -29 9 - 17* 10 98 -88 11 42 41 12 37 -35	H 7 2 1 76 -77 2 104 105 3 38 38 4 - 8* 5 - 4*	H 7 5 0 33 36 1 27 -29 2 20 -23 314* 4 63 -69 5 54 60 61* 8 1 35 -42 2 47 57 310* 6 30 -36 7 39 -49 87* H 7 7 0 21 26 116* 37* H 7 7 0 21 26 116* 318* 4 39 -58 5 28 40 1 51 50 61 59 3 65 -67 7 -58* 8 79 71 9 29 -15 10 82 88 11 40 -34 12 -23* H 9 1 12 -33 3 -40 1 29 -33 55 -51 1 7 -62 7 - 58* 8 79 71 9 29 -15 6 7 52 43 8 96 -83 98* 11 29 -33 8 96 -83 98* 11 20 44 12 35 40 1 7 1 67 2 70 66 7 52 43 8 96 -83 98* 11 20 44 12 35 40 1 71 67 2 70 66 7 52 43 8 96 -83 98* 11 27 10 67 2 70 66 7 52 73 8 96 -83 98* 11 25 44 12 35 40 17 1 67 2 70 66 2 58 -53 4 25 -18 5 62 -51 614*
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Table 2. Continued.

8	53	46	3	44	-46	н	9	4	5	-	-14#	5 42	49	4	22	-11
9	23	-20	4	53	50	1	48	48	10	43	67	6 36	-43			-36
10	64	67	5	65	60	2	49	47				7 23	30	6	-	~5*
11	41	-41	6	59	-55	3	46	-47	н	9	5	8 49	-61			
			7	48	48	4	-	-16*	0	-	- 22*					
	9	3		73				-45	1	-	-19*	н 9	6			
		-41	9	-	16*			- 8*			3*	1 3				
		-35	10	-	-3*			0.			-28	2 28				
2	-	- 4*	11	35	48	8	44	50	4	33	43	3 2	-36			

These were based on a data set consisting of 509 strong structure factors with k=2n and 313 weak structure factors with k=2n+1. Mean values of  $F_{hkl}$  and  $F_{\bar{h}kl}$  for k=2n were used, those reflexions that did not occur twice being eliminated. Positional parameters, including isotropic temperature factors, and layer scale factors were refined, only one of the four oxygen atoms  $O_7 - O_{10}$  being refined at a time. These four oxygen atoms were refined alternately until the shifts were negligible. This method of refinement was necessary owing to coupling between the x and y parameters of  $O_7 - O_{10}$ . Cruickshank's weighting scheme was used, and the refinement yielded a final R value of 0.061. The final R factor based on the strong structure factors was 0.046, while that based on the weak structure factors was 0.158.

No correction was made for anomalous dispersion since the data set consisted partly of reflexions obtained with copper and partly of reflexions obtained with molybdenum radiation.

The positional parameters were also refined with all atoms occupying the general position 4(c) in space group Pnn2. After several cycles of refinement, the parameter shifts had still not converged. The space group Pnnm was therefore considered to be the correct one.

Table 3. Atomic coordinates, expressed as fractions of the cell edges, and isotropic thermal parameters in Å<sup>2</sup>. Standard deviations are given within brackets.

Atom	Occ. number	x	$oldsymbol{y}$	z	В
Hf,	1	0.0505(1)	0.1246(3)	0	0.95(2)
$Hf_2$	1	0.0421(1)	0.6269(3)	0	0.88(2)
$\operatorname{Cr}_{1}$	1	0.3716(5)	0.1608(6)	0	1.1(1)'
$\operatorname{Cr}_{\mathbf{a}}^{1}$	1	0.3622(5)	0.5910(6)	0	1.1(1)
$Cr_3$	0.14	0.191(3)	$0.872(\hat{5})'$	0	1.2(6)
$O_1$	1	0.068(1)	0.134(2)	0.304(2)	1.3(3)
$O_2$	1	0.049(1)	0.628(3)	0.303(3)	1.7(3)
$O_3$	1	0.243(2)	0.110(2)	0`´	0.6(3)
$O_4$	1	0.227(2)	0.637(3)	0	1.5(4)
$O_{5}$	1	0.354(3)	0.276(3)	0	2.8(7)
$O_6$	1	0.351(4)	0.476(4)	0	4.4(11)
O,	1	0.107(2)	0.271(2)	0	1.6(4)
$O_8$	1	0.089(2)	0.775(2)	0	1.7(5)
O.	1	0.092(3)	0.963(2)	0	1.9(5)
O <sub>10</sub>	1	0.093(3)	0.467(2)	0	1.9(5)
$O_{11}$	0.14	0.282(12)	0.868(16)	0.184(22)	2.2(23)
O <sub>12</sub>	0.86	-0.305(5)	0.122(5)	0 ′	5.6(13)

Table 4. Distances (Å) and angles (°) in  $\sim \rm{Hf_4(OH)_8(CrO_4)_4.H_2O}$ . Standard deviations are given within parentheses.

	pentagonal bipyramid	ls:		
axial oxygen atoms: equatorial	$\rm Hf_1 - 2O_1$	2.10(2)	$\mathrm{Hf_2}\!-\!2\mathrm{O_2}$	2.08(2)
oxygen atoms:	$\begin{array}{l} Hf_1 - O_3 \\ Hf_1 - O_7 \\ Hf_1 - O_8 \\ Hf_1 - O_9 \\ Hf_1 - O_{9'} \end{array}$	2.24(2) 2.09(3) 2.12(3) 2.25(3) 2.03(3)	$\begin{array}{l} Hf_2 - O_4 \\ Hf_2 - O_7 \\ Hf_2 - O_8 \\ Hf_2 - O_{10} \\ Hf_2 - O_{10} \end{array}$	2.13(3) 2.21(3) 2.08(3) 2.25(3) 2.01(3)
	$\begin{array}{c} O_{1}-Hf_{1}-O_{1} \\ O_{3}-Hf_{1}-O_{7} \\ O_{7}-Hf_{1}-O_{8} \\ O_{8}-Hf_{1}-O_{9}' \\ O_{9}'-Hf_{1}-O_{9} \\ O_{9}-Hf_{1}-O_{3} \end{array}$	167(1) 77(1) 68(1) 76(1) 66(1) 73(1)	$\begin{array}{l} O_2 - Hf_2 - O_2 \\ O_4 - Hf_2 - O_8 \\ O_8 - Hf_2 - O_7 \\ O_7 - Hf_2 - O_{10} \\ O_{10} - Hf_2 - O_{10} \\ O_{10} ' - Hf_2 - O_4 \end{array}$	176(1) 71(1) 66(1) 78(1) 66(1) 78(1)
<b>ax.</b> – eq.:	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2.92(2) 2.82(3) 3.03(3) 3.13(4)	$O_2 - O_4$ $O_2 - O_7$ $O_2 - O_8$ $O_2 - O_{10}$	2.92(3) 3.07(3) 2.92(4) 3.06(4) 2.94(3)
eq. – eq.:	$O_1 - O_9$ $O_3 - O_7$ $O_7 - O_8$ $O_8 - O_9'$ $O_9' - O_9$ $O_9 - O_3$	3.08(3) 2.70(4) 2.34(4) 2.56(5) 2.34(6) 2.65(4)	$\begin{array}{c} O_2 - O_{10}' \\ O_4 - O_8 \\ O_8 - O_7 \\ O_7 - O_{10}' \\ O_{10}' - O_{10} \\ O_{10} - O_4 \end{array}$	2.46(5) 2.34(4) 2.67(5) 2.33(6) 2.78(5)
Within the CrO <sub>4</sub>	tetrahedra sharing ver	tices with HfO <sub>7</sub> :		
	$     \begin{array}{l}       \text{Cr}_1 - 2\text{O}_2 \\       \text{Cr}_1 - \text{O}_3 \\       \text{Cr}_1 - \text{O}_5     \end{array} $	1.69(2) 1.63(2) 1.57(4)	$     \begin{array}{l}       \text{Cr}_2 - 2\text{O}_1 \\       \text{Cr}_2 - \text{O}_4 \\       \text{Cr}_2 - \text{O}_6     \end{array} $	1.67(2) 1.68(3) 1.56(5)
	$ O_2 - Cr_1 - O_2 $ $ O_2 - Cr_1 - O_3 $ $ O_3 - Cr_1 - O_5 $ $ O_5 - Cr_1 - O_2 $	106(1) 112(1) 108(2) 109(1)	$\begin{array}{c} O_1 - Cr_2 - O_1 \\ O_1 - Cr_2 - O_4 \\ O_4 - Cr_2 - O_6 \\ O_6 - Cr_2 - O_1 \end{array}$	107(1) 108(1) 107(2) 113(1)
Within the CrO <sub>4</sub>	tetrahedra sharing an	edge with HfO	:	
	$\begin{array}{l} {\rm Cr_3 - O_8} \\ {\rm Cr_3 - O_9} \\ {\rm Cr_3 - 2O_{11}} \end{array}$	1.78(6) 1.69(6) 1.64(15)	$egin{array}{l} { m O_8 - Cr_3 - O_9} \\ { m O_9 - Cr_3 - O_{11}} \\ { m O_{11} - Cr_3 - O_8} \\ { m O_{11} - Cr_3 - O_{11}} \\ \end{array}$	95(2) 118(7) 113(7) 101(10)
Other distances:	${ m O}_{12}({ m H}_2{ m O}) - { m O}_8 \ { m O}_{12}({ m H}_2{ m O}) - { m O}_9{}'$	2.86(7) 2.71(7)	$ Hf_1 - Hf_1  Hf_1 - Hf_2  Hf_2 - Hf_2 $	3.581(9) 3.542(6) 3.583(9)

The observed and calculated structure factors together with those corresponding to the unobserved k=2n+1 reflexions are listed in Table 2. The atomic positions and their standard deviations are given in Table 3.

## DESCRIPTION OF THE STRUCTURE

4HfO<sub>2</sub>.4.3CrO<sub>3</sub>.5.4H<sub>2</sub>O is isomorphous with 4ZrO<sub>2</sub>.4.9CrO<sub>3</sub>.3.7H<sub>2</sub>O apart from the different Cr<sub>3</sub> chromate and water contents. The most important distances and angles are given in Table 4. To facilitate a comparison between the structures of the zirconium and hafnium chromates the labelling of the atoms and the lay-out of the table are the same as for 4ZrO<sub>2</sub>.4.9CrO<sub>3</sub>.3.7H<sub>2</sub>O.

The hafnium atoms are joined by double hydroxide bridges involving the oxygen atoms  $O_7 - O_{10}$ . Planar infinite chains of composition  $[Hf(OH)_2]_n^{2n+}$ , running parallel to the y axis, are thus formed. In addition, there are three oxygen atoms from three different chromate groups coordinated to each hafnium atom. All the hafnium atoms are thus seven coordinated the oxygen atoms being situated at the vertices of distorted pentagonal bipyramids. The chromate groups Cr<sub>1</sub> and Cr<sub>2</sub> each share three vertices with three HfO<sub>7</sub> polyhedra belonging to different chains. The chains are thus connected in the x and z directions to form a three-dimensional network. The structure described has the composition 4HfO<sub>2</sub>.4CrO<sub>3</sub>.6H<sub>2</sub>O if the two water molecules of crystallization are taken into account. The additional chromate groups, corresponding to the Cr<sub>3</sub> atoms, are situated in the same holes in the structure as the water molecules, though not simultaneously. Each CrO<sub>4</sub><sup>2-</sup> entering such a hole expels  $2OH^-$  in the  $[Hf(OH)_2]_n^{2n+}$  chain and thus shares one tetrahedron edge with a pentagonal bipyramid. The occupation number of  $O_{12}$ , as deduced from the Fourier synthesis, is very nearly 1 and the compound can therefore be formulated as  $4 \text{HfO}_2 \cdot (4+x) \text{CrO}_3 \cdot (6-2x) \text{H}_2 \text{O}$ . The x value may vary between 0 and 2 without changing the structure, since Z=2. For this crystal x was found to be 0.28.

In Fig. 1, approximately one formula unit of the structure is depicted in perspective with distances given in Å. The Hf-Hf distances are on an average  $3.56_2$  Å and are significantly shorter than the average Zr-Zr distance

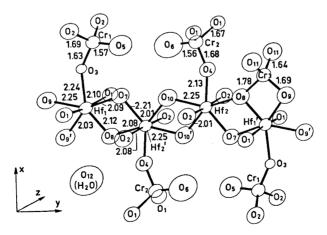


Fig. 1. One approximate formula unit of 4HfO<sub>2</sub>.4.3CrO<sub>3</sub>.5.4H<sub>2</sub>O shown in perspective. The thermal motions are outlined as spheres and the distances are given in Å.

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(3.597 Å) in zirconium chromate. Assuming that the O-Me-O angles in the  $Me-(OH)_2$  bridges are not altered, the short Hf-Hf distance results in a displacement of the bridging oxygen atoms in opposite directions in order to avoid too close an oxygen-oxygen contact. The Hf-O distances are hence alternately short and long, as can be seen from Table 4 and Fig. 1.

Since the structure is held together by chromate groups, there may be structural constraints on the chains due, for example, to the close contact (2.73 Å) between the chromate oxygen atoms  $O_5$  and  $O_6$ . However, due to experimental difficulties, the results obtained do not permit a more detailed comparison between this hafnium chromate and the structures of other similar zirconium and hafnium compounds.

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